



Stability analysis for the TPF interferometer

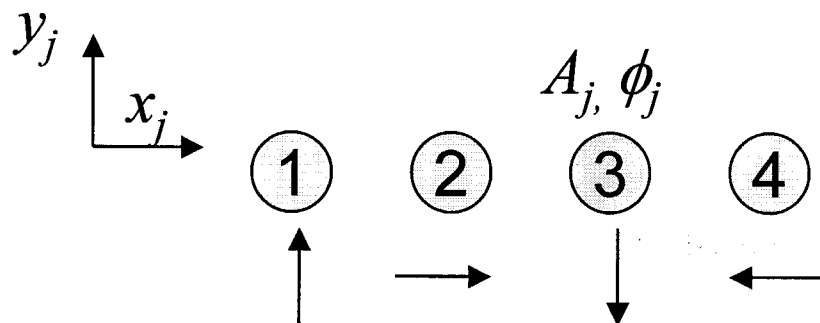
Oliver Lay

4/2/03

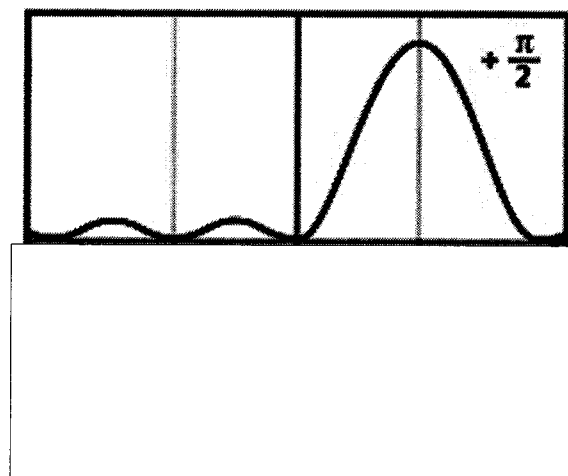
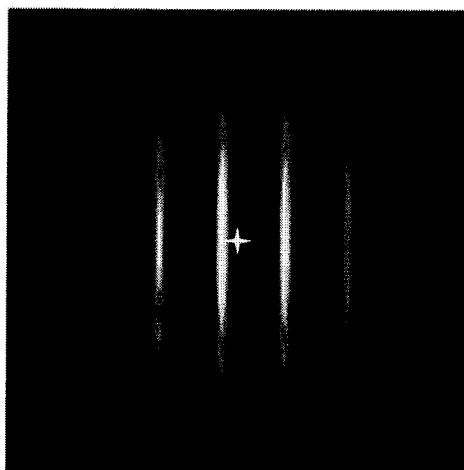
Jet Propulsion Laboratory
California Institute of Technology

- New class of mixed “bi-linear” errors identified which dominate the stability budget
- Not removed by phase chopping
- Leads to tolerances ~ 5 times tighter than those needed for 10^{-5} null depth:
 - Amplitude control $\sim 0.1\%$
 - Phase control ~ 1 nm
 - Approx. equivalent to requirements for 5×10^{-7} null depth
- Non-linear frequency mixing makes these difficult to calibrate
- Dual Bracewell used as example, but basic results apply to other configurations

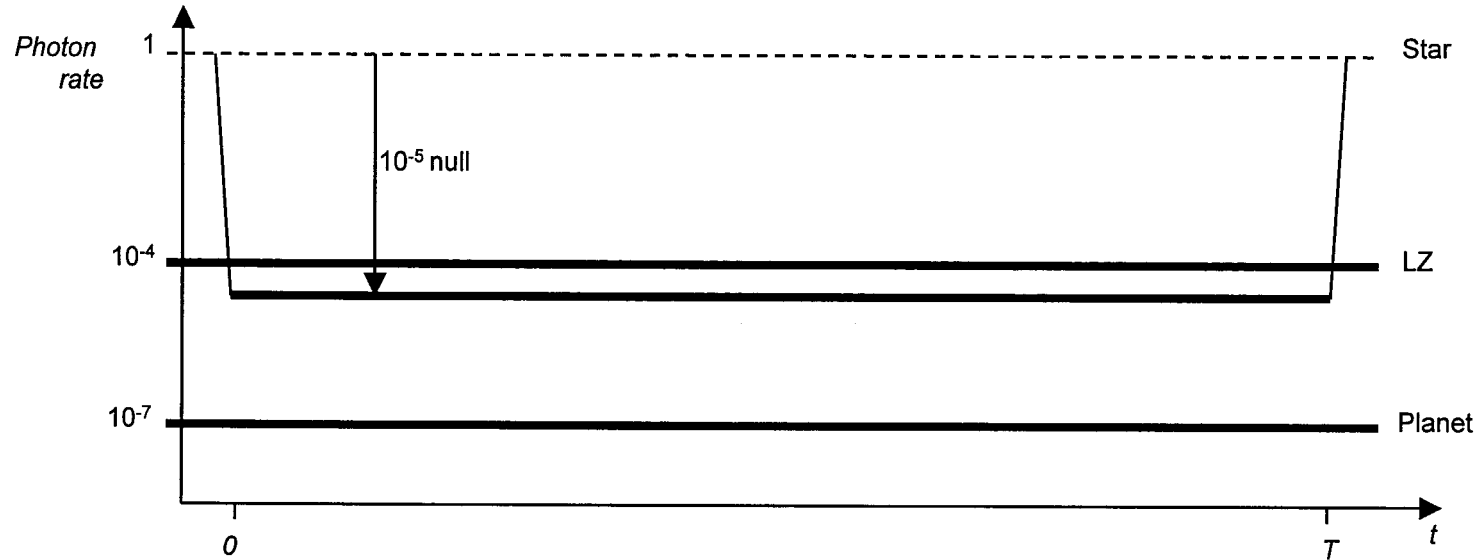
- Ability to isolate planet photons depends on:
 - Photon Shot noise
 - Detector gain variations
 - Thermal noise and scattered light
 - Polarization leakage
 - Null instability from E-field amplitude and phase imbalance
- This presentation is about the amplitude and phase balance. Contributors include:
 - Mirror surface figure
 - Pointing control
 - Delay tracking
 - Contamination of reflectivity
 - Dispersion effects
- The goal of this talk is to describe the new challenging requirements that have emerged




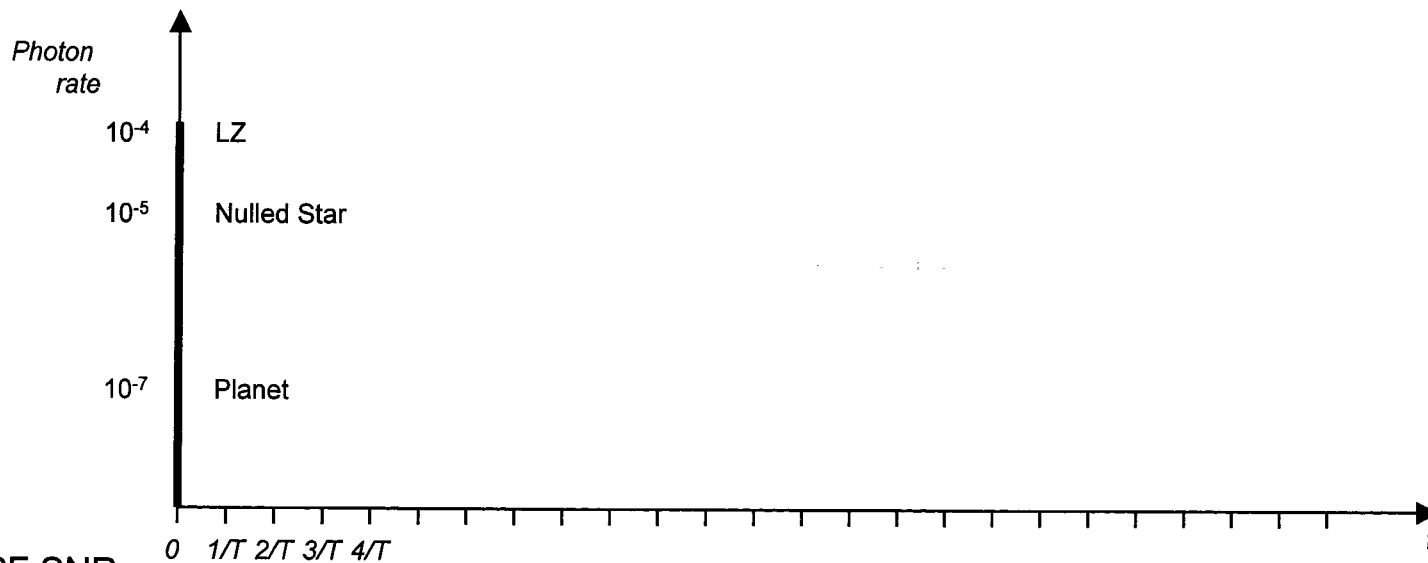
j	1	2	3	4
A_j	1	1	1	1
ϕ_j	0	$\pi/2$	π	$3\pi/2$



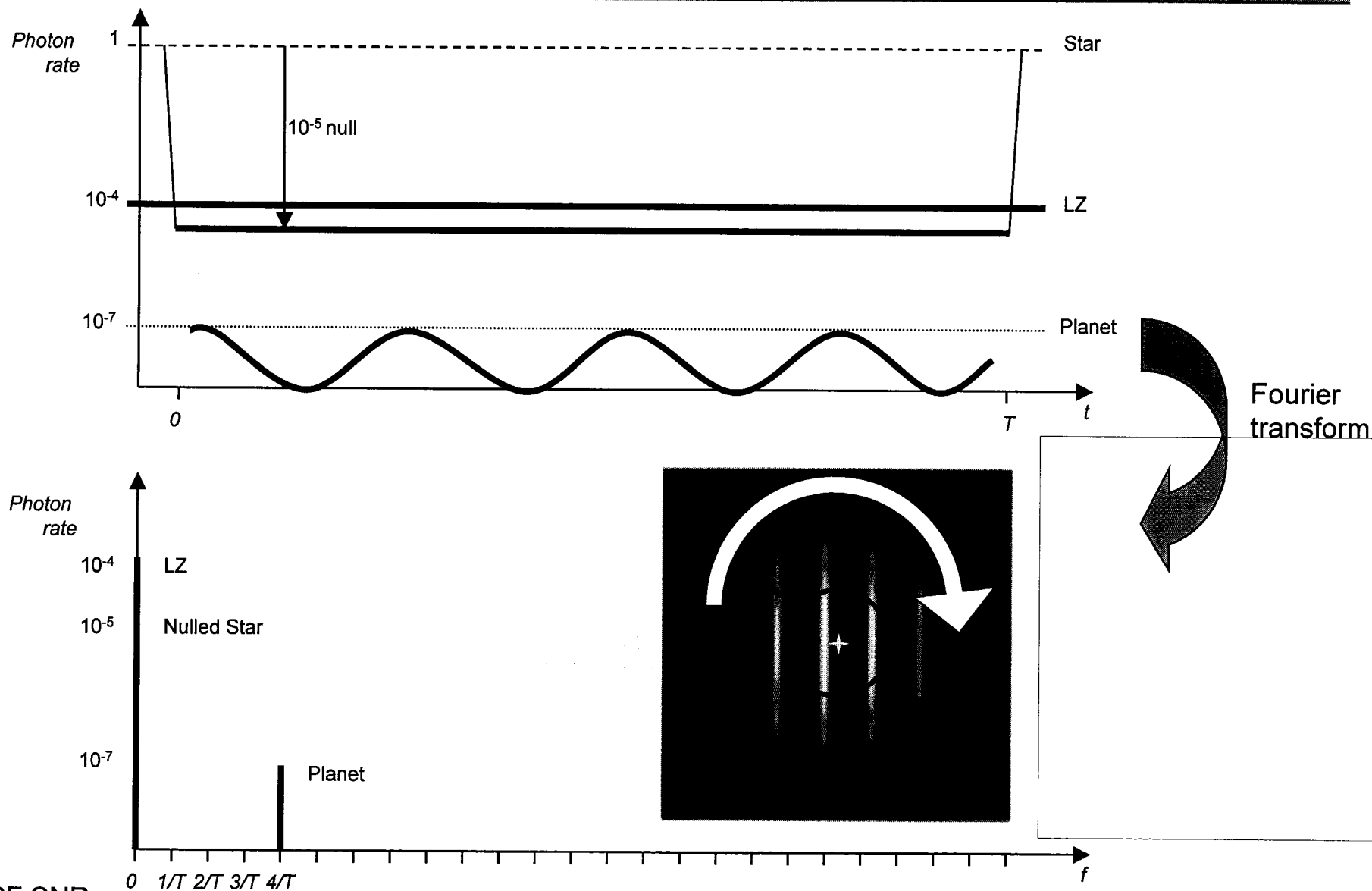
Prior view of stability requirements

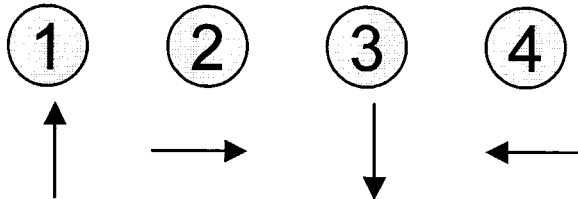


Fourier transform

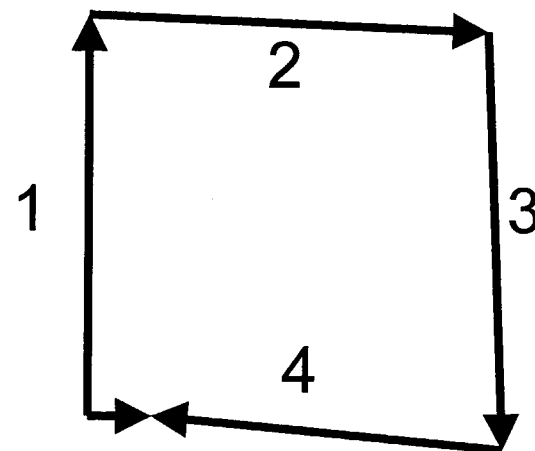
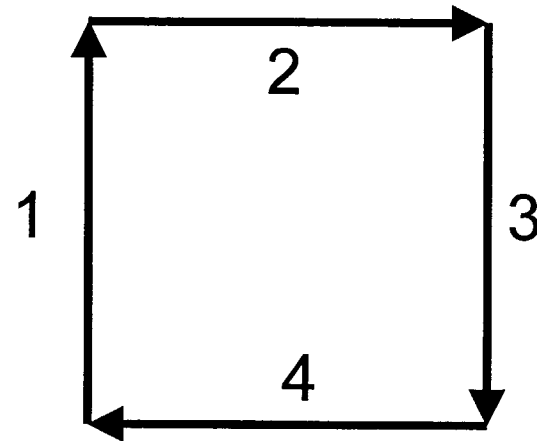



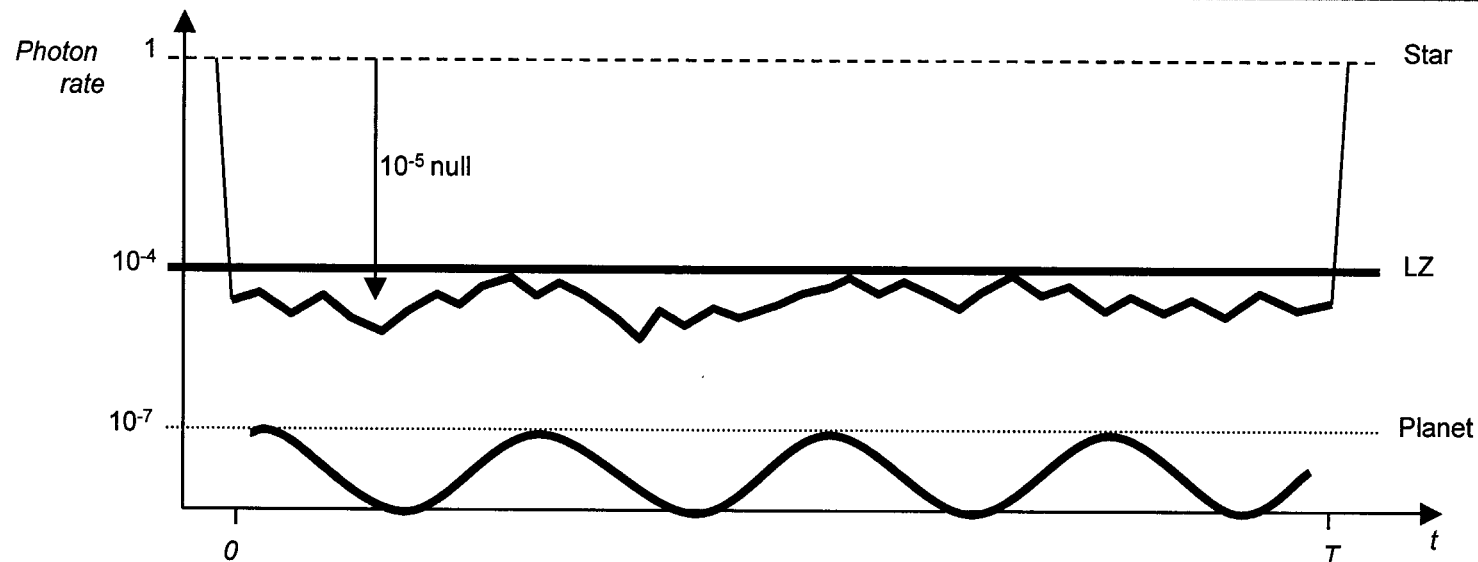
TPF SNR



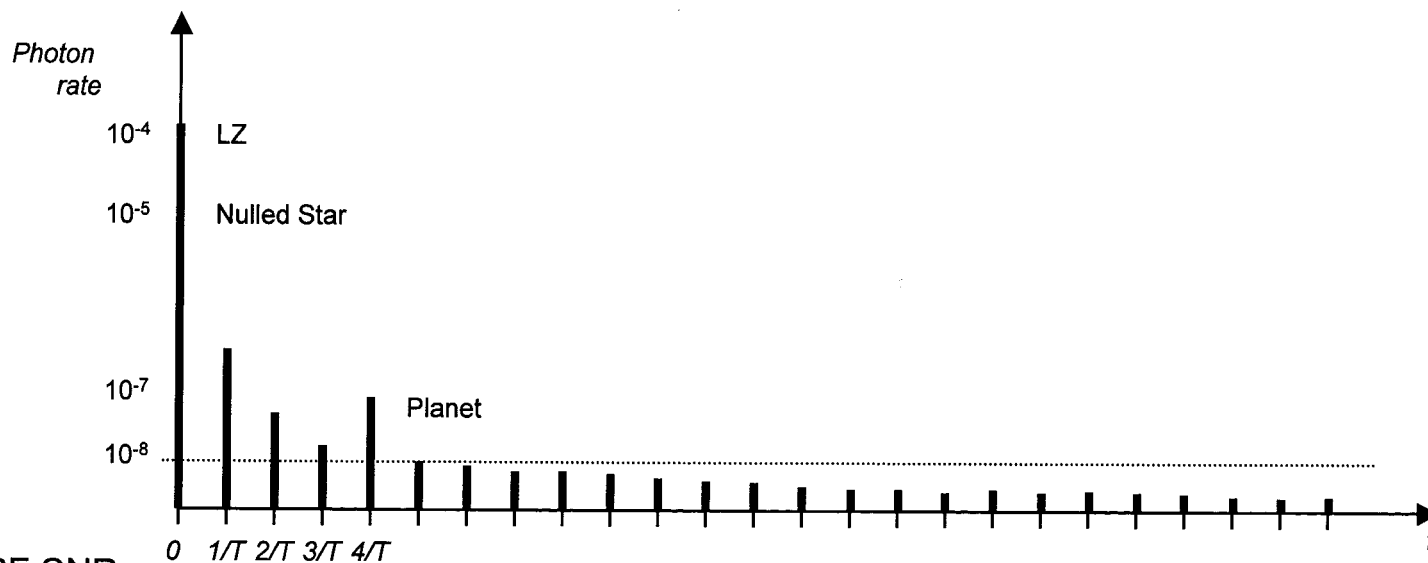


- A precarious balance of amplitudes and phases is holding back a deluge of stellar photons
- Any small perturbation in amplitude or phase changes number of stellar photons
 - e.g. mis-pointing, vibration, alignment drift, distortion of optical surfaces

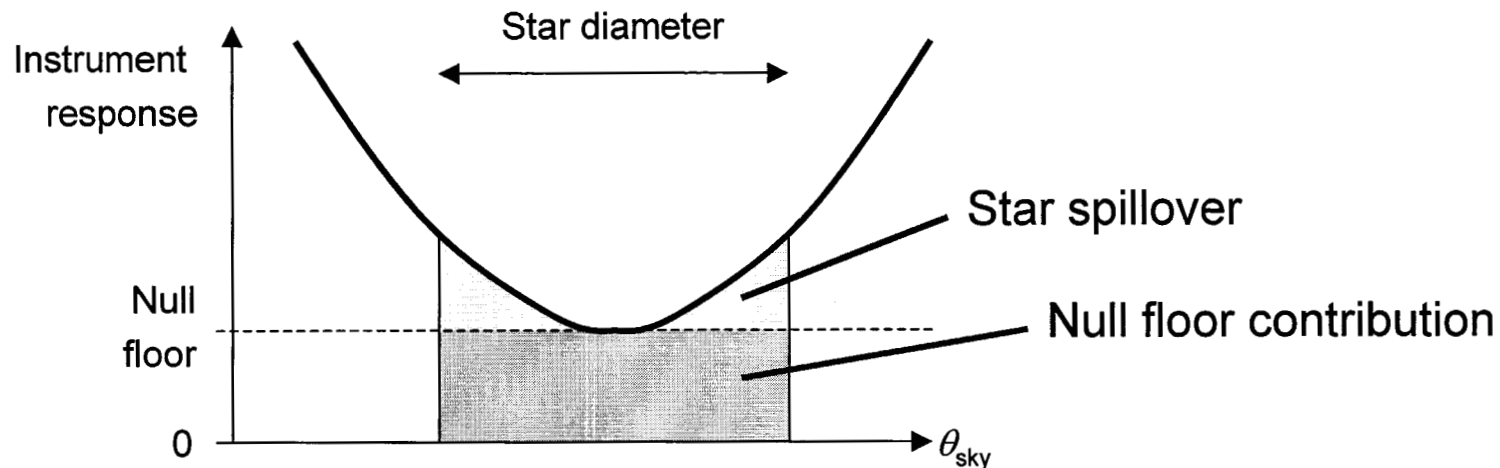




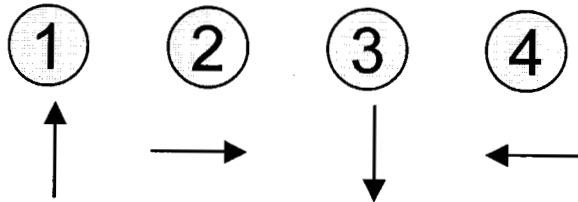
Fourier transform



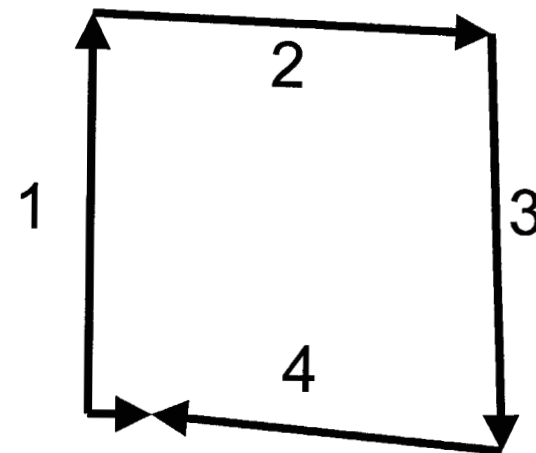
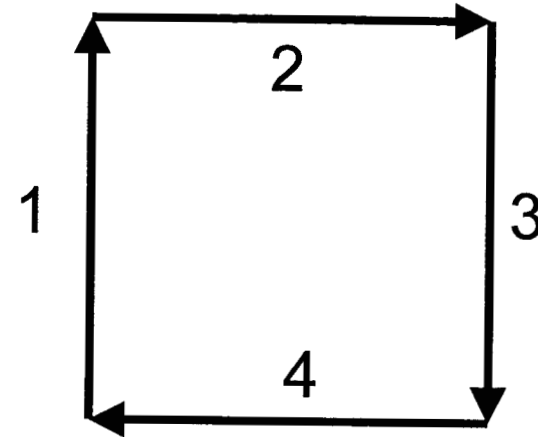
TPF SNR

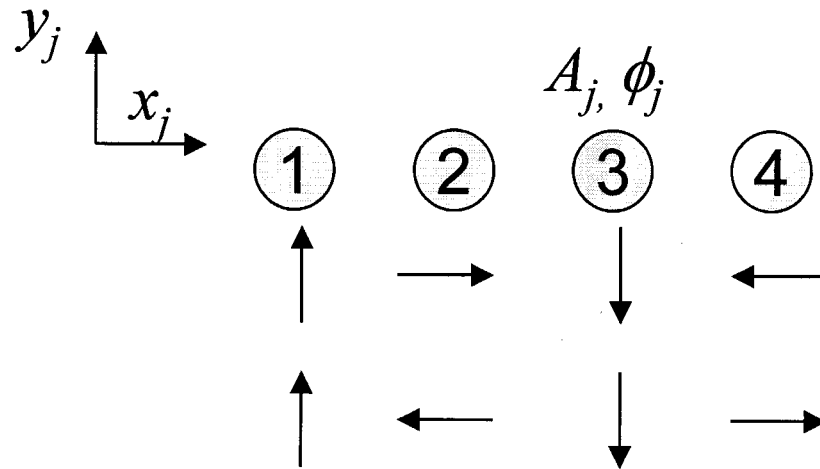


- Analysis covers both types of leakage
- “Null floor” effects dominate “Star spillover”
 - Tolerances derived here will be same for a point-like star
- A broad null does not help
 - Bracewell, OASES, etc. all approx. equally susceptible to amplitude & phase instabilities

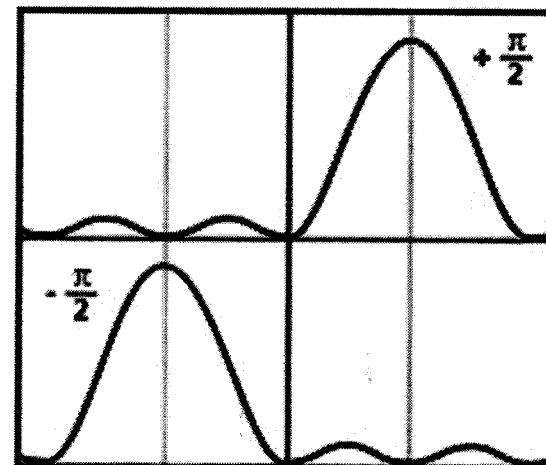
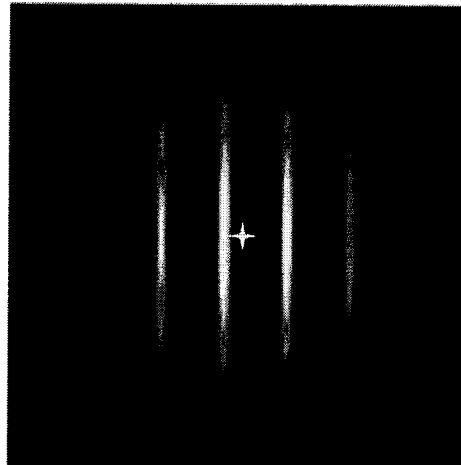


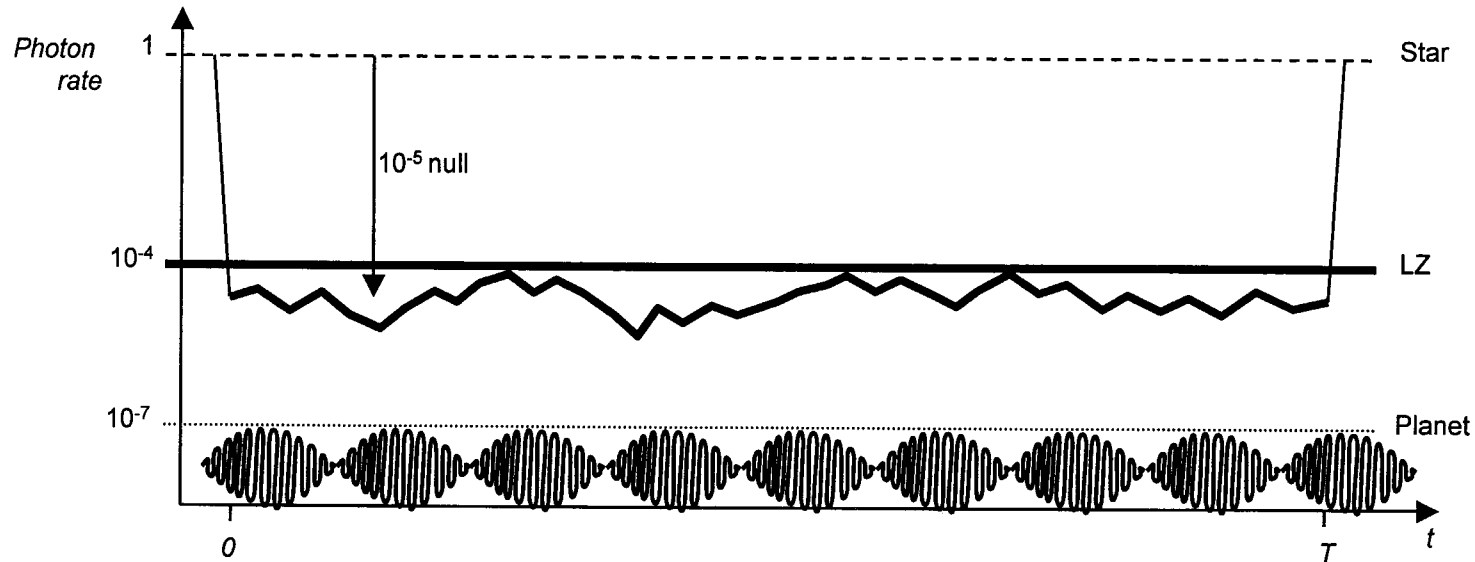
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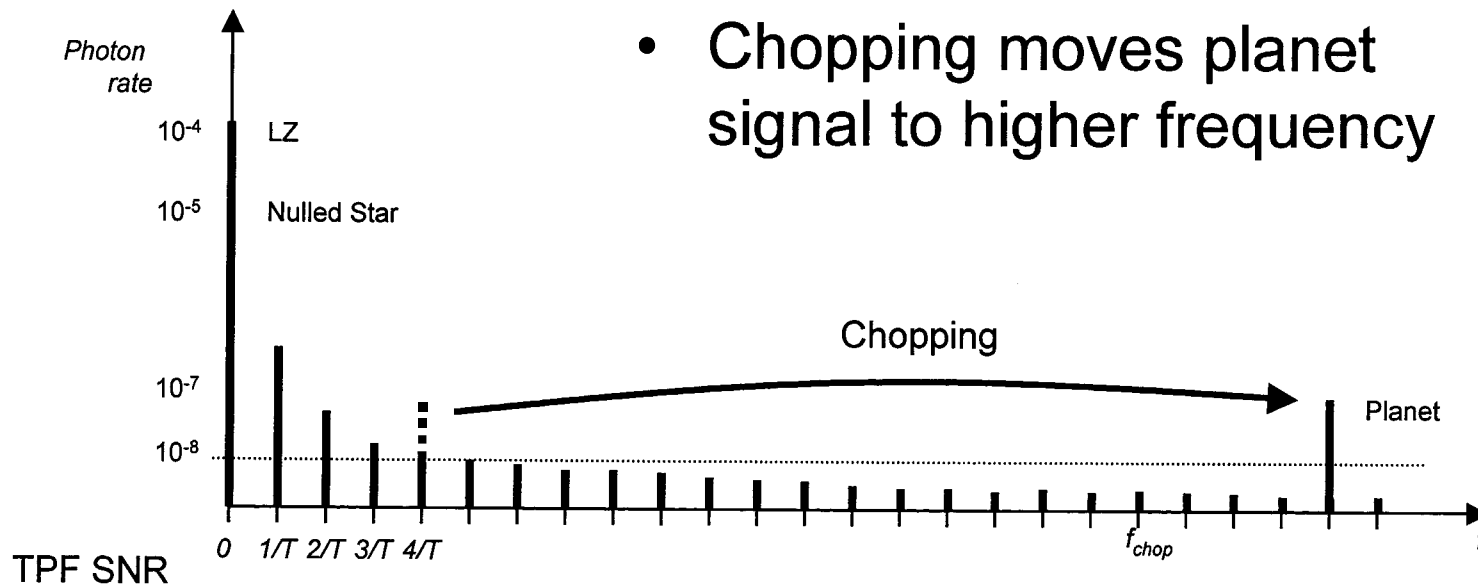
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A_j	1	1	1	1
ϕ_j	0	$\pi/2$	π	$3\pi/2$
ϕ_j'	0	$3\pi/2$	π	$\pi/2$



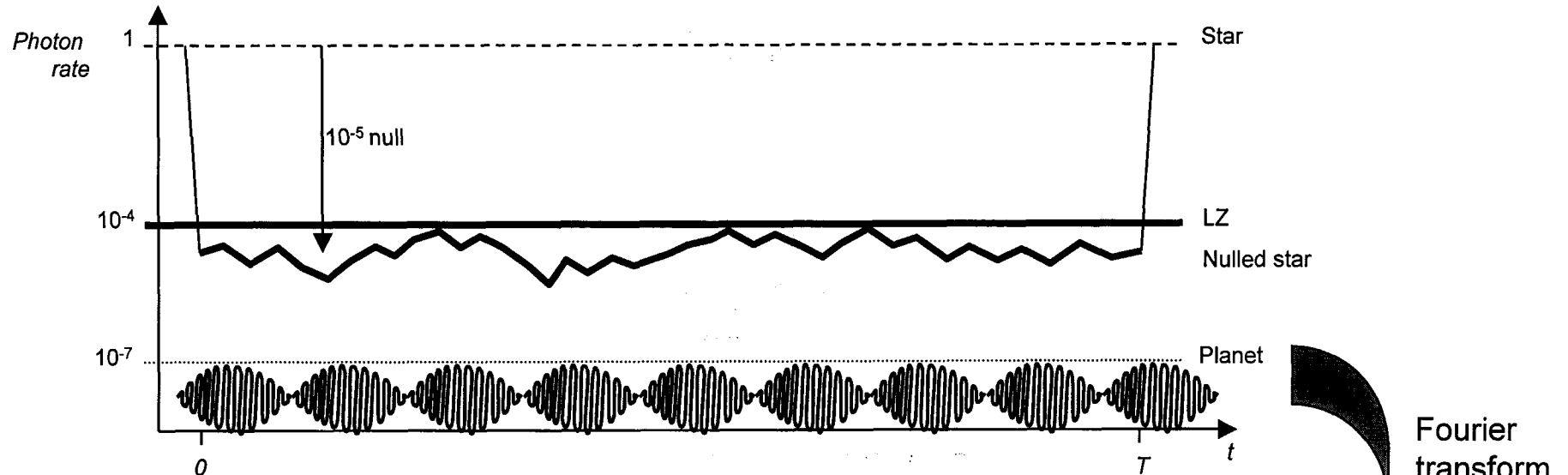


Fourier transform

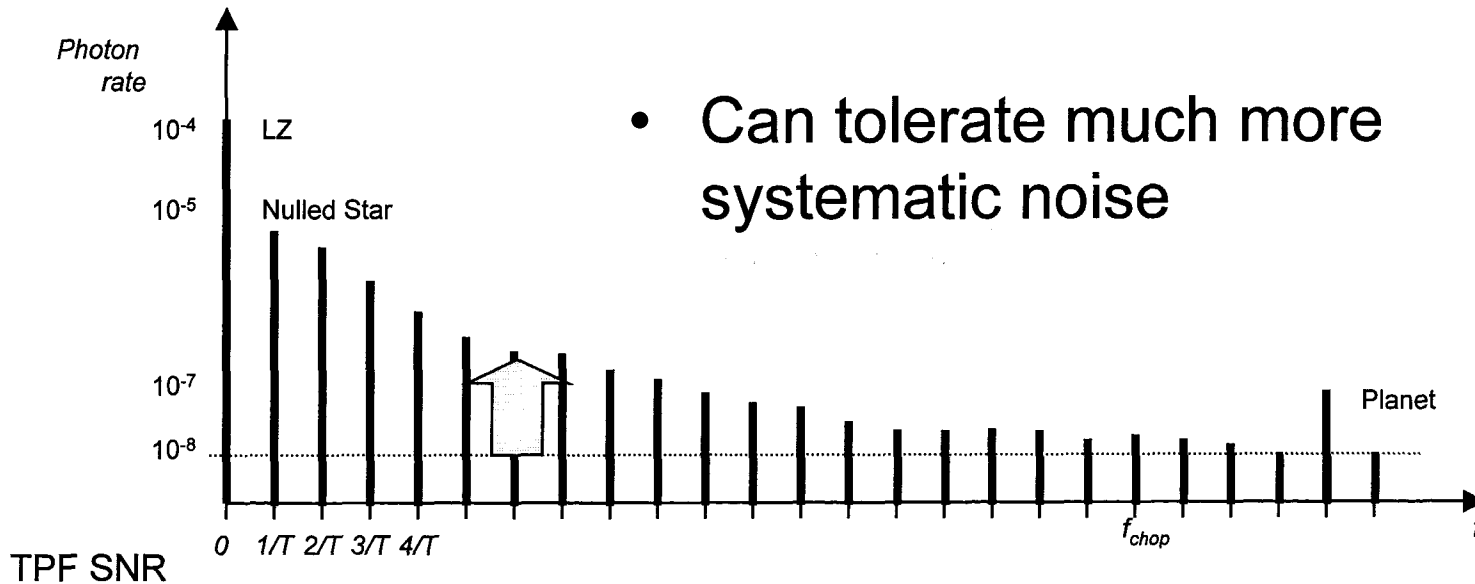
- Chopping moves planet signal to higher frequency



TPF SNR



- Can tolerate much more systematic noise



		Old	
		No chopping	With chopping
Photon noise (null depth)	δA	0.5%	0.5%
	$\delta \phi$	7 nm	7 nm
Systematic noise (null stability)	δA	0.13%	4%
	$\delta \phi$	2.0 nm	60 nm

Assumes 1/f noise

- Photon noise drives requirements on amplitude and phase error
- Assumes chop action does not introduce asymmetry

New view of stability requirements

- Stellar photon rate

$$X\left(\left\{A_j, \phi_j, x_j, y_j\right\}\right)$$

- Sensitivity of photon rate to perturbations of the variables obtained by differentiation:

$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j \right\}$$

- But $\{A_j, \phi_j\}$ have been chosen to minimize X , so these first derivatives are close to zero:

$$\frac{dX}{dA_j} \approx 0 \qquad \frac{dX}{d\phi_j} \approx 0$$

- Need to go to second order in these terms...

~~$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j + \frac{d^2 X}{dA_j^2} \delta A_j^2 + \frac{d^2 X}{d\phi_j^2} \delta \phi_j^2 \right\}$$~~

- Need to include the mixed 'bi-linear' terms, of which there are many:

$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j + \sum_k \left[\frac{1}{2} \frac{d^2 X}{dA_j dA_k} \delta A_j \delta A_k + \frac{d^2 X}{dA_j d\phi_k} \delta A_j \delta \phi_k + \frac{1}{2} \frac{d^2 X}{d\phi_j d\phi_k} \delta \phi_j \delta \phi_k \right] \right\}$$

- For 4 collectors we have 64 terms instead of 16

- Breakdown of noise contributions
(% of total noise variance):

$$\{\delta A_j\} \quad 5\%$$

$$\{\delta \phi_j\} \quad 1\%$$

$$\{\delta A_j \delta A_k\} \quad 20\%$$

$$\{\delta A_j \delta \phi_k\} \quad 53\%$$

$$\{\delta \phi_j \delta \phi_k\} \quad 20\%$$

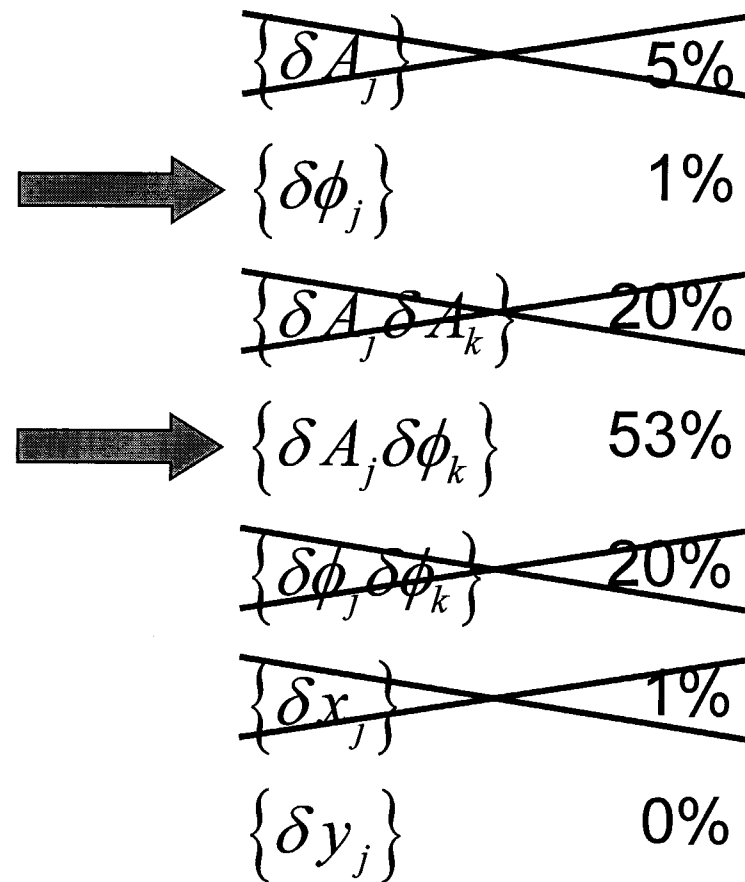
$$\{\delta x_j\} \quad 1\%$$

$$\{\delta y_j\} \quad 0\%$$











- Lo-res Dual Bracewell configuration, 40 m array length
- Solar system @ 10 pc
- Single spectral channel @ 10 μm
- Full rotation of the array
- $\delta A = 0.0005$ (0.05%)
- $\delta \phi = 0.0005$ rad (0.8 nm)
- $\delta x = 0.01$ m
- $\delta y = 0.01$ m
- Gives SNR = 2 (systematic noise only)

- Dominated by mixed, bi-linear terms, particularly amplitude-phase













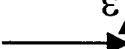




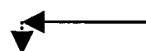


- Phase chopping removes some errors
- Breakdown of noise contributions (% of total noise variance):



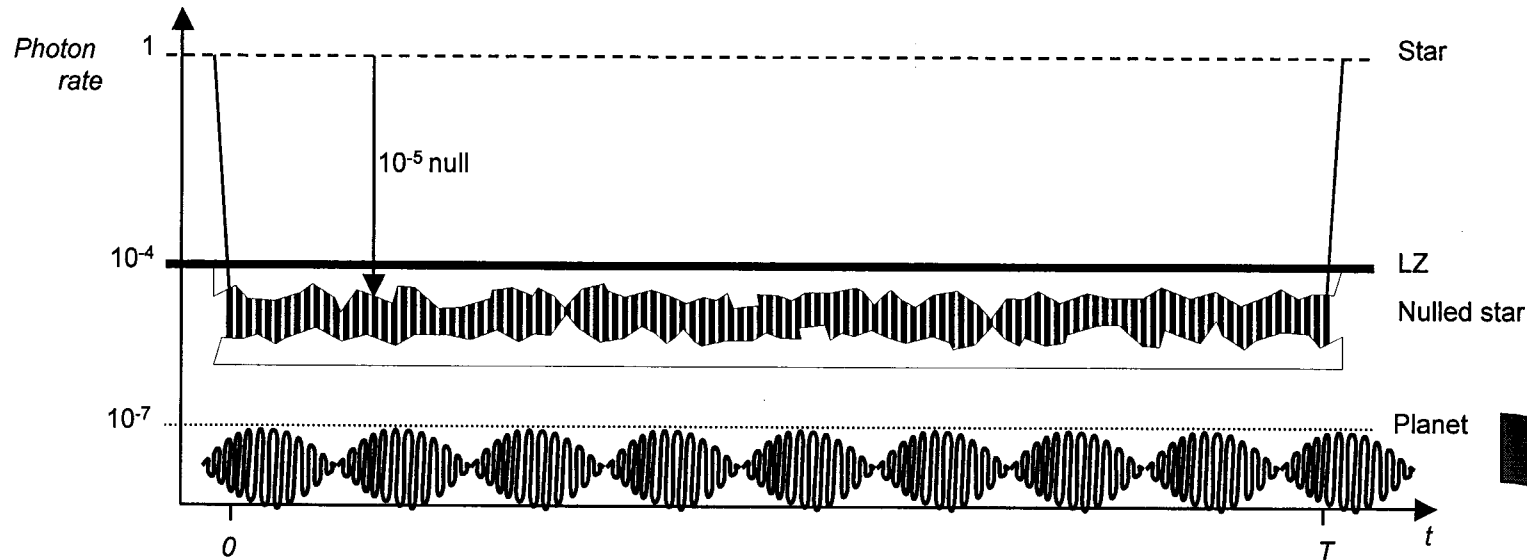
- But is ineffective against the new, dominant, mixed amp-phase terms

Error term	Chop state	Collector				Resultant phasor	Photon rate	Left - Right
		1	2	3	4			
δA_1^2	Left						ϵ^2	0
	Right						ϵ^2	

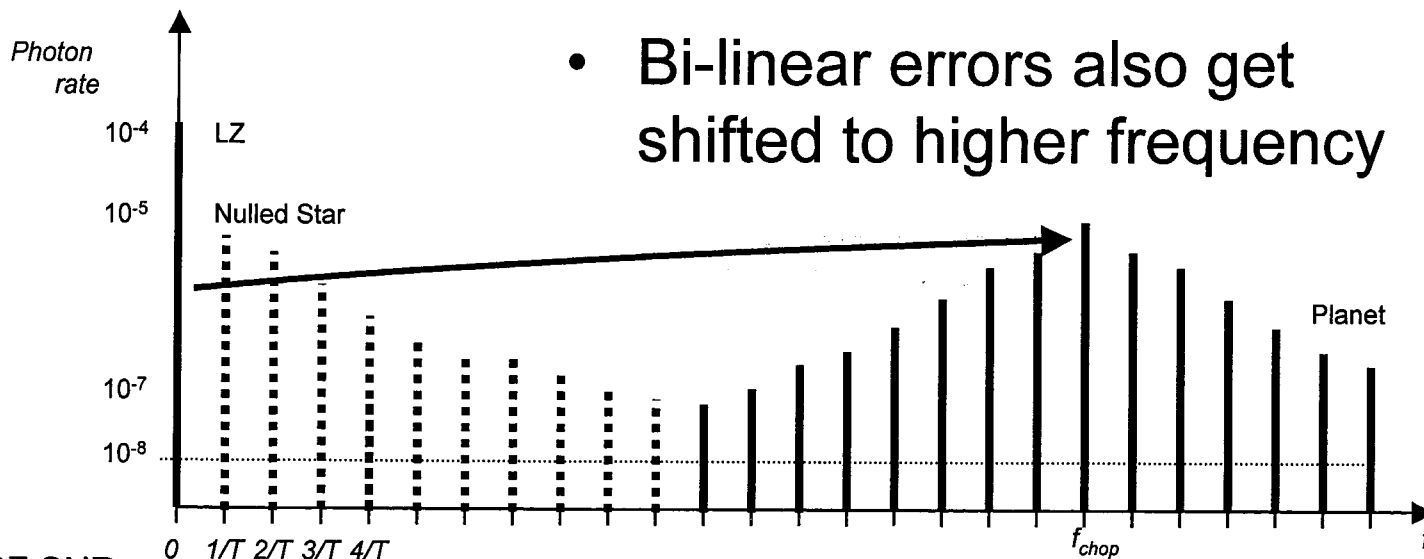
- This quadratic error is effectively suppressed by phase chopping

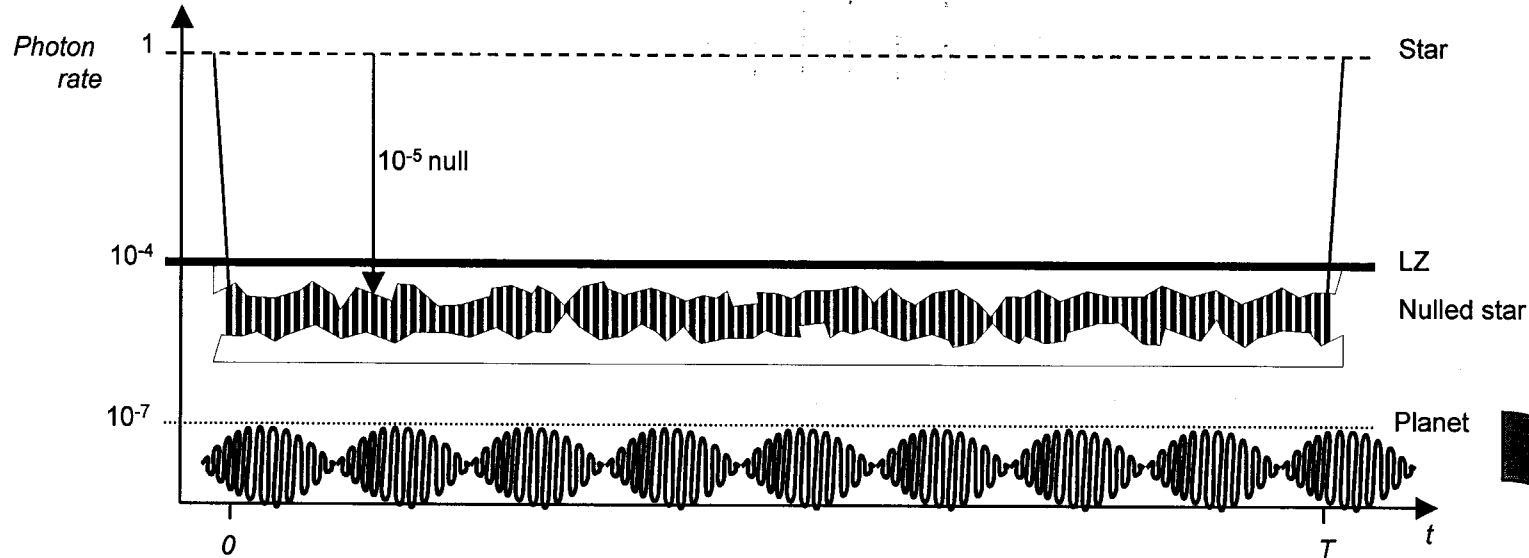
Error term	Chop state	Collector				Resultant phasor	Photon rate	Left - Right
		1	2	3	4			
δA_1^2	Left						ϵ^2	0
	Right						ϵ^2	
$\delta A_1 \delta \phi_3$	Left						$4\epsilon^2$	$4\epsilon^2$
	Right						0	

- ...but this bi-linear error is amplified



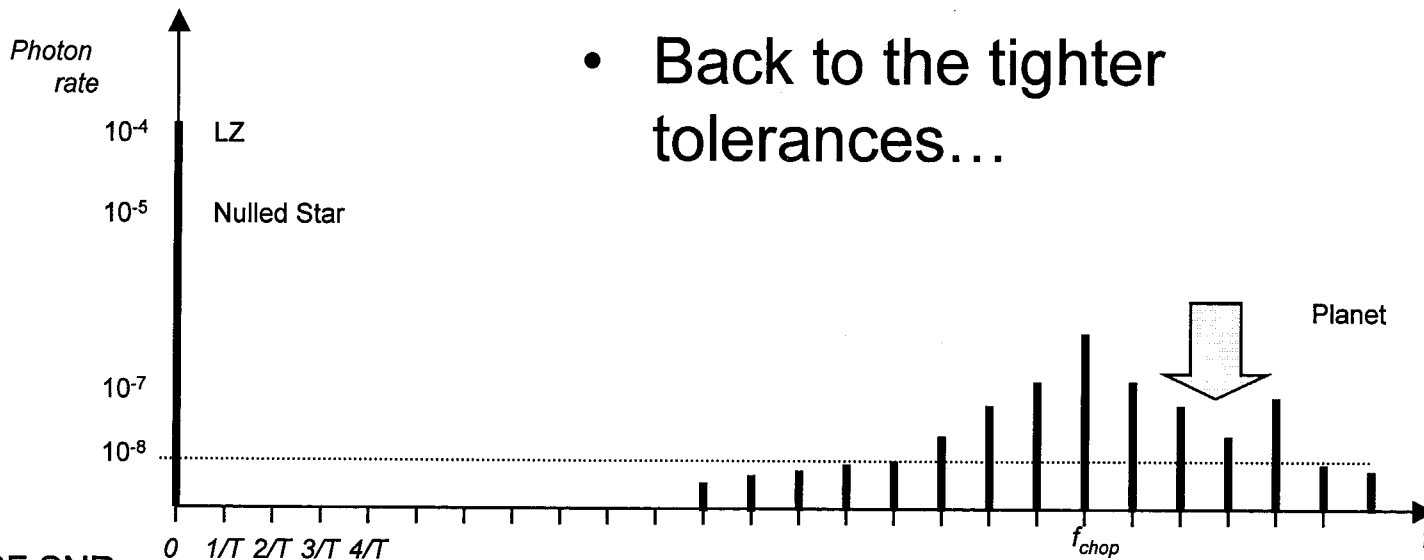
- Bi-linear errors also get shifted to higher frequency





Fourier transform

- Back to the tighter tolerances...



TPF SNR

		Old		New	
		No chop	Chop	No chop	Chop
Photon noise (null depth)	δA	0.5%	0.5%	0.5%	0.5%
	$\delta \phi$	7 nm	7 nm	7 nm	7 nm
Systematic noise (null stability)	δA	0.13%	4%	0.09%	0.1%
	$\delta \phi$	2.0 nm	60 nm	1.4 nm	1.5 nm

- Systematic noise drives requirements on amplitude and phase error, with or without phase chopping

$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j + \sum_k \left[\frac{1}{2} \frac{d^2 X}{dA_j dA_k} \delta A_j \delta A_k + \frac{d^2 X}{dA_j d\phi_k} \delta A_j \delta \phi_k + \frac{1}{2} \frac{d^2 X}{d\phi_j d\phi_k} \delta \phi_j \delta \phi_k \right] \right\}$$

- Null stability is dominated by non-linear terms
- For a linear term:
 - fluctuations in A_1 at 0.1 mHz cause fluctuations in photon rate at 0.1 mHz
- Bi-linear terms: mixing between perturbations!!
 - fluctuation in A_1 at 5.4 mHz and a fluctuation in ϕ_3 at 5.3 mHz mix to give a fluctuation in X at 0.1 mHz
- Entire PSD for amplitude and phase contributes to each fluctuation frequency in photon rate
- Means that regular calibration of amplitude and phase has limited effect

- They are requirements on control, not just knowledge
- They apply to all frequencies, including DC
 - not a particular frequency range
 - PSD shape has some impact
- They apply across a factor of 3 in wavelength and to both polarizations
- Tolerances relax only as $T^{1/4}$
- Cannot use null depth for sensing
 - Not enough SNR to detect variations 5 times weaker than planet
- So must measure amplitudes for individual beams and phases between pairs

		New	
		No chop	Chop
Systematic noise (null stability)	δA	0.09%	0.1%
	$\delta \phi$	1.4 nm	1.5 nm

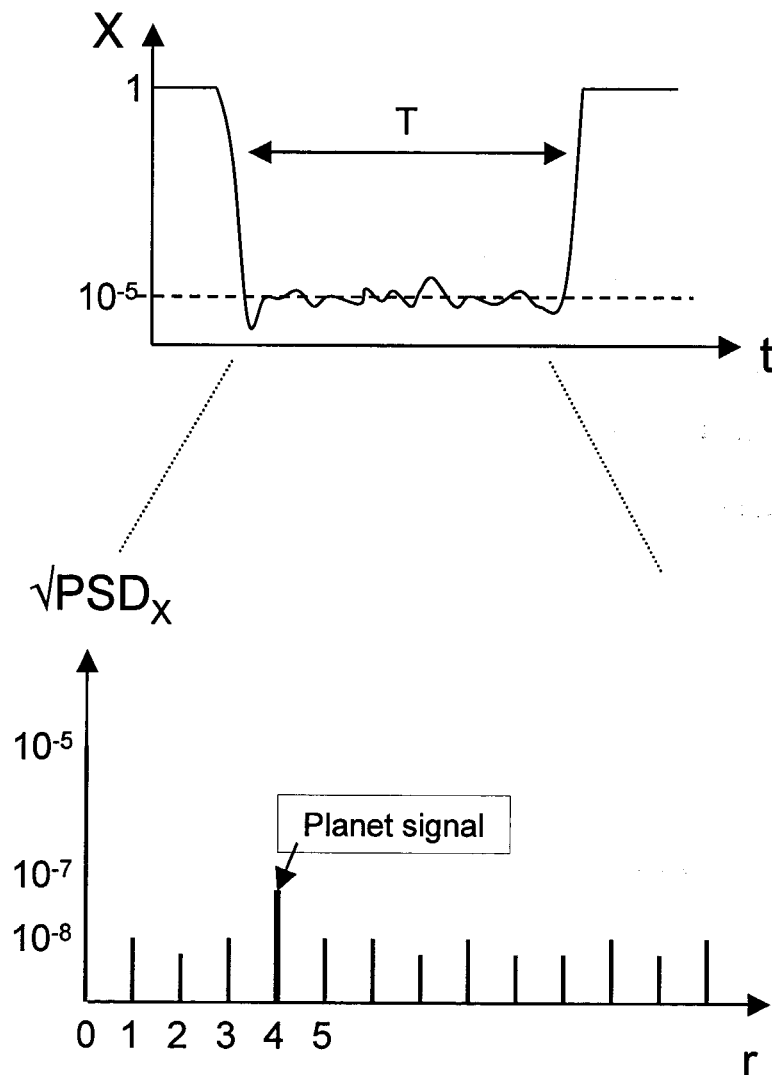
3 possibilities:

- Show that new analysis is incorrect
- Find an observable for a nulling configuration that is much less sensitive to amplitude and phase perturbations
- Identify an approach to controlling amplitude to 0.1% and phase to ~ 1.5 nm

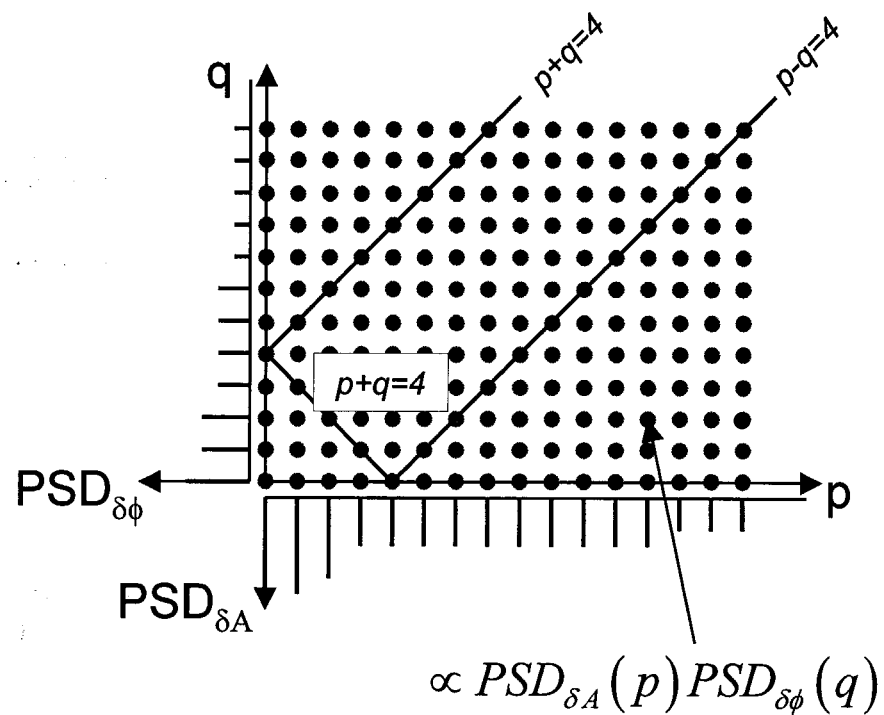
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- Non-linear frequency mixing makes these difficult to calibrate
- Dual Bracewell used as example, but basic results apply to other configurations

Back-up slides

- Rapid rotation of the array
 - Tolerances on δA and $\delta\phi$ go as $f_{rot}^{-1/4}$
- Regular monitoring and correction of A and ϕ
 - Perfect calibration every 100 s only relaxes tolerances by factor ~ 2.5
- Use full $0-2\pi$ sweep of phase before cross-combiner
 - Does not help since planet and star both have same sinusoidal signature



$\delta A \delta \phi$ contribution:



$$\delta X \approx \sum_j \left\{ \sum_k \left[\frac{1}{2} \frac{d^2 X}{dA_j dA_k} \delta A_j \delta A_k + \frac{d^2 X}{dA_j d\phi_k} \delta A_j \delta \phi_k + \frac{1}{2} \frac{d^2 X}{d\phi_j d\phi_k} \delta \phi_j \delta \phi_k \right] \right\}$$

$$X\left(\left\{A_j, \phi_j, x_j, y_j\right\}\right) \quad \delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j \right\}$$

$$\frac{dX}{dA_j} \approx 0 \quad \frac{dX}{d\phi_j} \approx 0$$

$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j + \frac{d^2 X}{dA_j^2} \delta A_j^2 + \frac{d^2 X}{d\phi_j^2} \delta \phi_j^2 \right\}$$

$$\delta X \approx \sum_j \left\{ \frac{dX}{dA_j} \delta A_j + \frac{dX}{d\phi_j} \delta \phi_j + \frac{dX}{dx_j} \delta x_j + \frac{dX}{dy_j} \delta y_j + \sum_k \left[\frac{1}{2} \frac{d^2 X}{dA_j dA_k} \delta A_j \delta A_k + \frac{d^2 X}{dA_j d\phi_k} \delta A_j \delta \phi_k + \frac{1}{2} \frac{d^2 X}{d\phi_j d\phi_k} \delta \phi_j \delta \phi_k \right] \right\}$$